



# Prediction of geotechnical properties of treated fibrous peat by artificial neural networks

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## Abstract

This paper concentrates on measuring the geotechnical properties of cement peat mixed with different dosages of well-graded sand as filler. Several geotechnical tests, namely unconfined compression strength (UCS), California bearing ratio (CBR) and compaction, were performed on the treated fibrous peat samples. The filler was used in a wide range of 50 to 400 kg/m<sup>3</sup> of wet peat. In addition, time-dependent changes of geotechnical properties of treated peat were also studied after 14, 28 and 90 days of air curing. Besides, different artificial neural networks trained by a back-propagation algorithm (ANN-BP) and particle swarm optimization method (ANN-PSO) were used to estimate the UCS of stabilized fibrous peat. Results indicate that after a 90-day curing period, the UCS and CBR of treated samples with 300-kg/m<sup>3</sup> cement only, increased by a factor as high as 8.54 and 13.66, respectively, compared to untreated peat. Besides, in the compaction tests, adding filler content to the cement peat increased the maximum dry density (MDD) significantly. In addition, the results of soft computing techniques indicated that the performance indices of the ANN-PSO model was better compared to the ANN-BP model. Finally, sensitivity results showed that the filler content and curing time were the most influential factors on estimating UCS.

**Keywords** Fibrous peat · Stabilization tests · Cement · Natural filler · CBR · Artificial neural network

## Introduction

Fibrous peats are an unconsolidated organic material since they are loosely arranged and their particles are not cemented

together. Mostly, they have accumulated under water in acidic conditions (Huat et al. 2014). These problematic soils can be found throughout the world. Almost 8% of the Earth's land is covered with peat (Mesri and Ajlouni 2007). These soils are classified as fibrous when the fiber and organic content is more than 66% and 75%, respectively (ASTM 2000). In sub-grade construction, they are generally considered as problematic soils because of their high compressibility and low shear strength properties in their natural state (Huat 2004). These kind of soils cannot be useful for foundation floors (Edil 2003). In particular, these extremely acidic soils are made of organisms, animals and fresh fibers (Kalantari and Prasad 2014). As a result, high permeability, high rates of creep and low pH are the other geotechnical properties of the peats. Additionally, due to high in situ void ratios of the peats (7.5 to 30), the in situ water content of these soils ranges from 500 to 2000%, respectively (Moayedi et al. 2014).

A great volume of research works has been performed to evaluate the effect of cement on the strength properties of peats (Table 1). However, the research to date has tended to focus on peat soil stabilization using different binders rather than filler effect. Regarding the filler effect, Celik and Canakci

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**Table 1** Studies conducted on the peat soil stabilization using cement

| Soil specification (average)   | Location   | Test details   | Results   |
|--|------------|--|---|
| Fibrous peat ( $H_3$ to $H_7$ ), untreated UCS = 14.23 kPa, pH = 5, (Kolay et al. 2011)      | Malaysia   | Cement was added at OWC 28-day water curing  | No optimum in UCS results was observed, UCS increased by OPC increment 20% OPC, increased the UCS to 115 kPa  |
| Fibrous peat, untreated UCS = 28 kPa Cc = 3.64 (Kalantari et al. 2010)                       | Malaysia   | Cement was added at field water content (198%-417%) after 90-day air curing 5% to 50% OPC was used   | 25% OPC, increased the UCS to 330 kPa   |
| Fibrous peat, untreated UCS = 54 kPa (Boobathiraja et al. 2014)                              | India      | Cement was added at OWC 10% to 50% OPC was used  | 25% OPC, increased the CBR to 25%<br>50% OPC, increased the UCS to 125 kPa  |
| Fibrous peat, water content = 1400% (Axelsson et al. 2002)                                   | Sweden     | The stabilized samples were subjected to the dispersed pressure of 18 kPa after 28- days air curing 50 kg/m <sup>3</sup> to 250 kg/m <sup>3</sup> OPC was used | 250 kg/m <sup>3</sup> OPC, increased the UCS to 300 kPa<br>Addition of 100 kg/m <sup>3</sup> sand gave an increment of 30 kPa in shear strength     |
| Sphagnum ( $H_6$ ), water content = 210% (Francisco and Al Tabbaa 2004)                      | Ireland    | 100 to 500 kg/m <sup>3</sup> OPC was used (relative to the wet mass of peat) 28 days and 90-days air curing  | Range of 300 – 400 kg/m <sup>3</sup> cement was proposed for peats (W/C = 1)  |
| Fibrous peat ( $H_4$ ), untreated UCS = 2 kPa, organic content = 96% (Hashim and Islam 2008) | Malaysia   | 300-kg/m <sup>3</sup> OPC + sodium bentonite (85:15) + 25% sand Air curing   | After 7 days curing, UCS reached to 37 kPa  |
| Irish fibrous peats, untreated UCS = 20 kPa (Hebib and Farrell 2003)                         | Ireland    | 150,200 and 250 kg/m <sup>3</sup> OPC (relative to the wet mass of peat) 28 and 90-day water curing  | 150,200 and 250 kg/m <sup>3</sup> OPC raised UCS of untreated peat to around 200,220 and 500 kPa, respectively                                      |
| Fibrous peat, untreated UCS = 28 kPa (Kalantari and Prasad 2014)                             | Malaysia   | UP to 50% OPC with three different curing method: (i) air (ii) water (iii) water + surcharge load (10 kPa) (28,90 and 180-days)                                | Water curing method with surcharge load gave the highest UCS values with 50% OPC  |
| Fibrous peat, water content = 697% (EuroSoilStab 2002)                                       | Netherland | 7 and 28-days water curing 200 and 400 kg/m <sup>3</sup> OPC (relative to the wet mass of peat) mixed with slag  | 200 and 400 kg/m <sup>3</sup> OPC mixed with slag increased UCS of untreated peat to around 400 and 600 kPa, after 7-day water curing, respectively |
| Banting peat ( $H_1$ to $H_6$ ) (Alwi 2008)  | Malaysia   | Cement and Bentonite (85:15) selected dosages: 250 Water curing 56-days  | 300-kg/m <sup>3</sup> cement with 41% sand, increased the UCS up to 425 kPa   |
| Fibrous peat ( $H_4$ ) (Deboucha et al. 2008)  | Malaysia   | 15% cement, 15% sand and 70% peat - Water curing for 56-days   | Increased the CBR from 10% to 25%   |

Note: OWC = optimum water content, OPC = ordinary Portland Cement, UCS = unconfined compression strength, CBR = California bearing ratio

(2014) evaluated the geotechnical characterizations of fibrous peat mixed with natural filler. In their study, the effects of filler dosages on compaction, shear strength and compressibility of fibrous peat were investigated. In the sample preparation, the untreated soil was mixed with filler at its maximum dry density (MDD) and optimum water content (OWC). Their results indicate that when the sand content increases in the peat, internal friction angle increases while the cohesion of the peat is reduced. Moreover, the compression ratio of the fibrous peat is marginally reduced when the filler content is increased.

The objective of this study is to discuss the effects of natural filler dosages on the geotechnical characterization of the treated peat samples. In addition, this study focuses on finding the optimum or proper filler range to improve the engineering properties of fibrous peat stabilized with cement using different geotechnical tests. Finally, an expert artificial neural network (ANN) trained with particle swarm optimization method is employed to estimate the UCS of treated peat samples from the other geotechnical properties such as California bearing ration, cement content, filler content, MDD and optimum water content.

### Experimental study

In this study, Undisturbed and disturbed peat samples were obtained from the Pontian area of the state of Johor in Malaysia. To get the undisturbed peat samples a special cylindrical tube with an internal diameter of 150 mm and with a height of 230 mm was used. Based on Von Post (Von 1992) classification system the peat was H<sub>3</sub>. In the present study, a total of 11 tests on unimproved peat samples and 90 tests on the stabilized peat samples were prepared at various binder compositions and dosages. It should be noticed that, in order to evaluate the filler effect, all the stabilization tests were carried out with fixed cement content of 300 kg/m<sup>3</sup> relative to wet mass of peat with different dosages of fillers. This amount was derived based on previous studies on the UCS of treated samples (Dehghanbanadaki et al. 2017). In case, we performed unconfined compressions (hereafter UCS) tests based on BS 1377:1990: Part 7: section 7 (British Standard Institution 1990) under strain control condition with the rate of 0.0125 mm/s. California bearing ratio (CBR) tests and compaction tests were carried out on treated samples based on ASTM D 1883-07E02 and ASTM D-698 (1992), respectively. In this research, for each experimental test two samples were prepared cured and tests and the average result of the tests was considered as final result. Table 2 summarizes the geotechnical properties of materials used in this study. Table 3 shows the detail of mix designs of each test. Grain size distributions of fibrous peat and filler used in this study are shown in Fig. 1 while, Fig. 2 demonstrates the sample preparation in this research. It should be mentioned that the details of sample

**Table 2** Properties of the peat, filler and cement used in this study (Dehghanbanadaki et al. 2013 & Dehghanbanadaki et al. 2017)

| Item                             | Results                   |
|----------------------------------|---------------------------|
| Peat                             |                           |
| WC %                             | 495                       |
| OC (%)                           | 91                        |
| pH                               | 4.1                       |
| Classification                   | Fibrous (H <sub>3</sub> ) |
| Unit weight (kN/m <sup>3</sup> ) | 10                        |
| Permeability (m/day)             | 0.89                      |
| Specific gravity                 | 1.38                      |
| C <sub>c</sub>                   | 3                         |
| C <sub>α</sub> (average)         | 0.065                     |
| LL                               | 260                       |
| C <sub>u</sub> – VST (kPa)       | 11                        |
| C <sub>u</sub> – UCS (kPa)       | 10                        |
| FC (%)                           | 80                        |
| Void ratio                       | 11                        |
| Filler (SW)                      |                           |
| Item                             | Results                   |
| MDD                              | 17.51                     |
| Friction angle                   | 36.8                      |
| Minimum void ratio               | 0.32                      |
| Specific gravity                 | 2.64                      |
| Fineness modulus                 | 2.81                      |
| Cement                           |                           |
| Item                             | Content (%)               |
| CaO                              | 68.6                      |
| SiO <sub>2</sub>                 | 21.6                      |
| Al <sub>2</sub> O <sub>3</sub>   | 5.3                       |
| Fe <sub>2</sub> O <sub>3</sub>   | 3.3                       |
| MgO                              | 1.1                       |
| SO <sub>3</sub>                  | <0.01                     |
| Na <sub>2</sub> O                | <0.01                     |
| K <sub>2</sub> O                 | <0.01                     |

Note: WC: in situ water content of the peat; OC: organic content; VST: vane shear test, C<sub>c</sub>: compression index; C<sub>α</sub>: secondary compression index; LL: liquid limit; C<sub>u</sub>: undrained shear strength; FC: fiber content; MDD: maximum dry density (kN/m<sup>3</sup>)

preparation for the tests can be found in previous publication (Dehghanbanadaki et al. 2017).

### Simulation by ANN models

#### Details of ANN

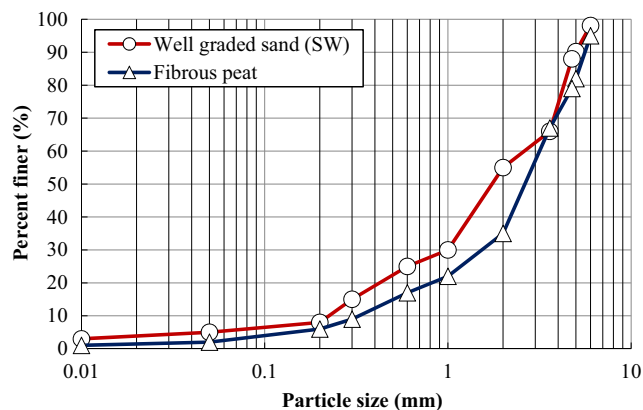
ANNs are considered very powerful tools to estimate any indistinct functional data (Rojas 2013; Maren et al. 2014; Baughman and Liu 2014). Therefore, for the estimation purposes, we used MATLAB R2016a software (nftool) to train

**Table 3** Mix designs of the stabilized peat specimens

| Number of tests | Test details   | Curing time (days) |
|-----------------|--|--------------------|
| 5               | UCS: UP  | –                  |
| 21              | UCS: UP + C (150, 200, 250, 300, 325, 350 and 400 kg/m <sup>3</sup> )    | 14, 28 and 90      |
| 3               | UCS: UP + C (300 kg/m <sup>3</sup> )                                     | 14, 28 and 90      |
| 3               | UCS: [UP + C (300 kg/m <sup>3</sup> )] + F (50 kg/m <sup>3</sup> )       | 14, 28 and 90      |
| 3               | UCS: [UP + C (300 kg/m <sup>3</sup> )] + F (75 kg/m <sup>3</sup> )       | 14, 28 and 90      |
| 3               | UCS: [UP + C (300 kg/m <sup>3</sup> )] + F (100 kg/m <sup>3</sup> )      | 14, 28 and 90      |
| 3               | UCS: [UP + C (300 kg/m <sup>3</sup> )] + F (125 kg/m <sup>3</sup> )      | 14, 28 and 90      |
| 3               | UCS: [UP + C (300 kg/m <sup>3</sup> )] + F (175 kg/m <sup>3</sup> )      | 14, 28 and 90      |
| 3               | UCS: [UP + C (300 kg/m <sup>3</sup> )] + F (200 kg/m <sup>3</sup> )      | 14, 28 and 90      |
| 12              | Compaction: UP + C (150, 200, 250, 300 kg/m <sup>3</sup> )               | 14, 28 and 90      |
| 3               | Compaction: UP   | –                  |
| 3               | Compaction: UP + C (300 kg/m <sup>3</sup> ) + F (50 kg/m <sup>3</sup> )  | 14, 28 and 90      |
| 3               | Compaction: UP + C (300 kg/m <sup>3</sup> ) + F (100 kg/m <sup>3</sup> ) | 14, 28 and 90      |
| 3               | Compaction: UP + C (300 kg/m <sup>3</sup> ) + F (150 kg/m <sup>3</sup> ) | 14, 28 and 90      |
| 3               | Compaction: UP + C (300 kg/m <sup>3</sup> ) + F (200 kg/m <sup>3</sup> ) | 14, 28 and 90      |
| 3               | CBR: UP  | –                  |
| 3               | CBR: UP + C (300 kg/m <sup>3</sup> )                                     | 14, 28 and 90      |
| 3               | CBR: UP + C (300 kg/m <sup>3</sup> ) + F (50 kg/m <sup>3</sup> )         | 14, 28 and 90      |
| 3               | CBR: UP + C (300 kg/m <sup>3</sup> ) + F (75 kg/m <sup>3</sup> )         | 14, 28 and 90      |
| 3               | CBR: UP + C (300 kg/m <sup>3</sup> ) + F (100 kg/m <sup>3</sup> )        | 14, 28 and 90      |
| 3               | CBR: UP + C (300 kg/m <sup>3</sup> ) + F (125 kg/m <sup>3</sup> )        | 14, 28 and 90      |
| 3               | CBR: UP + C (300 kg/m <sup>3</sup> ) + F (150 kg/m <sup>3</sup> )        | 14, 28 and 90      |
| 3               | CBR: UP + C (300 kg/m <sup>3</sup> ) + F (175 kg/m <sup>3</sup> )        | 14, 28 and 90      |
| 3               | CBR: UP + C (300 kg/m <sup>3</sup> ) + F (200 kg/m <sup>3</sup> )        | 14, 28 and 90      |

- UP: untreated peat, C: cement, F: filler, UCS: unconfined compression strength, CBR: California bearing ratio.
- UP + C (300 kg/m<sup>3</sup>) = untreated peat mixed with 300-kg/m<sup>3</sup> cement only.
- UP + C (300 kg/m<sup>3</sup>) + F (50 kg/m<sup>3</sup>) = at first: untreated peat mixed with 300-kg/m<sup>3</sup> cement then 50 kg/m<sup>3</sup> well-graded sand as filler was added to the mixture.

and develop different ANN models. Briefly, different multi-layer feed-forward perceptron (MLP-FF) networks trained by Levenberg–Marquardt (LM) backpropagation (BP) were adopted, while for the transfer function, we selected a logistic sigmoid function. In the MLP models, CBR, curing time, filler



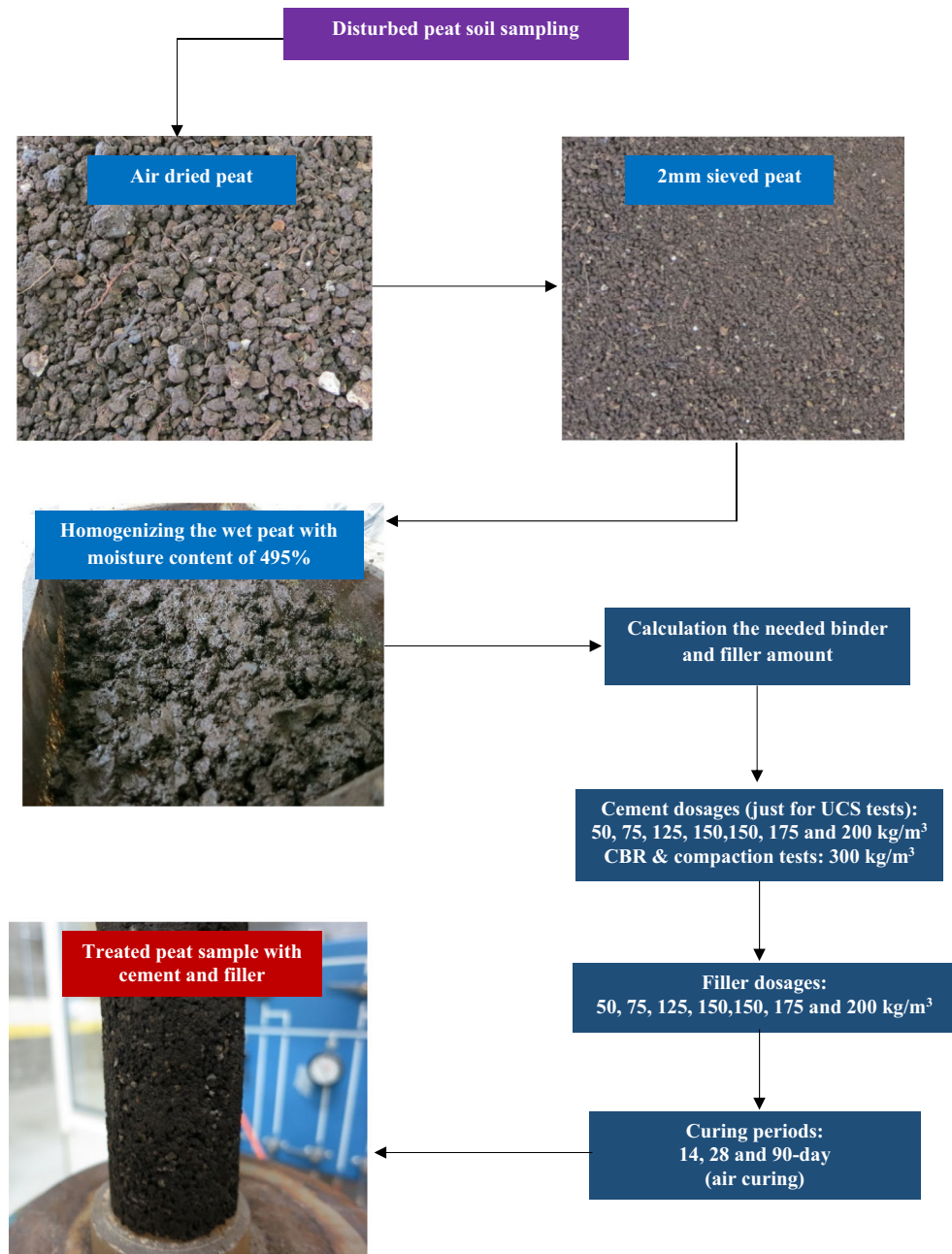
**Fig. 1** Grain size distributions of soil and filler (Dehghanbanadaki et al. 2017)

content, OWC and MDD were considered as inputs, whereas UCS was selected as the target of the ANN. In data classification, we followed the method proposed by Shahin et al. (2004) with 70% of data for training, 15% for validating and 15% for testing was considered. Finally, for error analysis, we used mean square error (*MSE*) and a coefficient of correlation (*R*). The MLP details of this study are shown in Fig. 3.

### Implementation of particle swarm optimization in MLP training

One of the drawbacks of the BP algorithm is a slow training rate and trapping in local minima (Jadav and Panchal 2012; Momeni et al. 2014). Several smart and evolutionary algorithms such as particle swarm optimization (PSO) algorithm, imperialist competitive algorithm (ICA), genetic algorithm (GA), bacterial foraging optimization technique (BFOT) and bee colony (BC) algorithm can be applied as a training methods in ANNs (Nanda and Panda 2014; Sun and Xu 2016). These population-based algorithms with

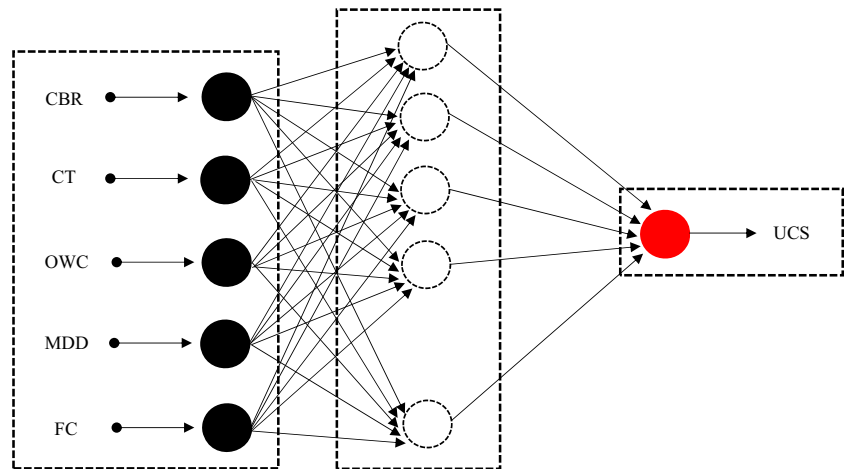
**Fig. 2** Sample preparation in this research (Dehghanbanadaki et al. 2017)



approximately similar concepts can improve the performance of the ANN models. Each agent in the population competes and shares the information to achieve certain tasks and better performance (Rahmanian et al. 2012). Consequently, in this paper, we selected PSO which is a population-based stochastic algorithm to increase the accuracy rate of the best ANN-MLP (BP) model. This smart algorithm was first proposed by Kennedy and Eberhart (1995). The training improvement performance of ANN-MLP models using PSO technique have been proven by several researchers (Zhang et al. 2007; Zamani and Sadeghian 2010; Hajihassani 2013; Sun and Xu 2016). the following items briefly show the implementation of the PSO algorithm in training of MLPs.

- Determination of PSO parameters (pre-defined coefficients, acceleration constants & coefficient of inertia weight)
- Random population of ANN weights & biases using vector-encoding technique
- Evaluation of cost function – *MSE* (mean square error) of ANN trained by BP
- Finding the local & global best of each particle  
If:
- Improvement in fitness for a certain number of iterations is not observed = termination
- Using ANN-PSO  
Else:
- Updating the particles

**Fig. 3** MLP model of this study. Note: CBR = California bearing ration, CT = curing time, OWC = optimum water content, MDD = maximum dry density and FC = filler content



## Results and discussions

### UCS tests results

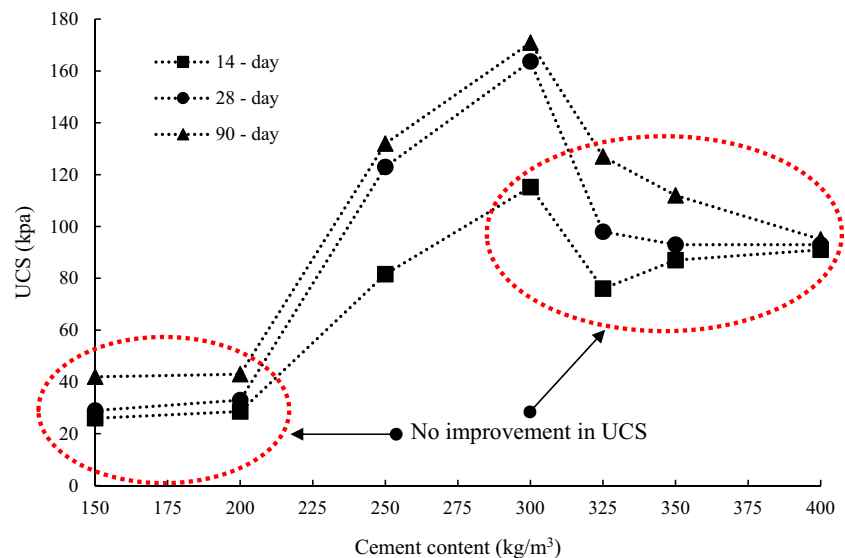
Figure 4 shows the UCS of treated peat samples at different cement dosages after 14-, 28- and 90-day curing periods. As can be seen, since the initial water content of the peat is fixed during the stabilization process, when the cement content was in the range of 150 to 200 and 300 to 400, no improvement in UCS was observed. Besides, it is evident from past studies that the UCS of treated peat samples with 300-kg/m<sup>3</sup> cement dosages should give higher shear strength compared to this research (Axelsson et al. 2002; EuroSoilStab 2002; Hebib and Farrell 2003; Alwi 2008, Kalantari et al. 2010; Motamedi et al. 2015). A possible explanation for this difference might be that the fibrous peat soil in this research has a high organic content of 91% which can impede the cement stabilization process significantly. In contrast, the achieved UCS values of treated peat samples were consistent with the results of Hashim and

Islam (2008). They stabilized the Malaysian fibrous peat with low shear strength (UCS = 2 kPa) and high organic content (96%) with 300-kg/m<sup>3</sup> cement + sodium bentonite (85:15) + 25% sand an using air-curing technique. They gained 37 kPa for the UCS of treated peat after 7-day air curing. To evaluate the degree of improvement of the stabilized soil, the UCS results were compared to Table 4 as proposed by Terzaghi et al. (1996). The optimum amount of filler content to increase the strength of cement peat was determined to be 125 kg/m<sup>3</sup> based on previous research of the first author (Dehghanbanadaki et al. 2013). Therefore, using this optimum amount (125 kg/m<sup>3</sup>) mixed with 300-kg/m<sup>3</sup> cement increased the UCS of untreated peat up to 944% after a 90-day curing time. This finding corroborates the results of Wong et al. (2013).

### CBR and compaction tests results

The trend of CBR changes of cement peat mixed with various percentages of filler content is presented in this section.

**Fig. 4** UCS of treated peat samples at different cement dosages



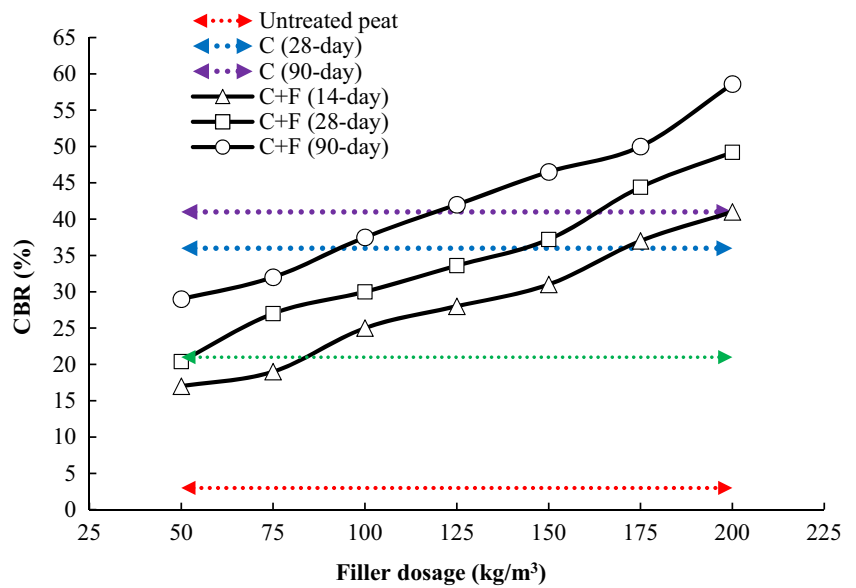
**Table 4** Consistency classification

| Consistency | UCS (kPa) | This study     |
|-------------|-----------|----------------|
| Very soft   | < 24      | 20 (untreated) |
| Soft        | 24-50     |                |
| Medium      | 50-100    |                |
| Stiff       | 100-200   | 170 (improved) |
| Hard        | 200-400   |                |
| Very hard   | > 400     |                |

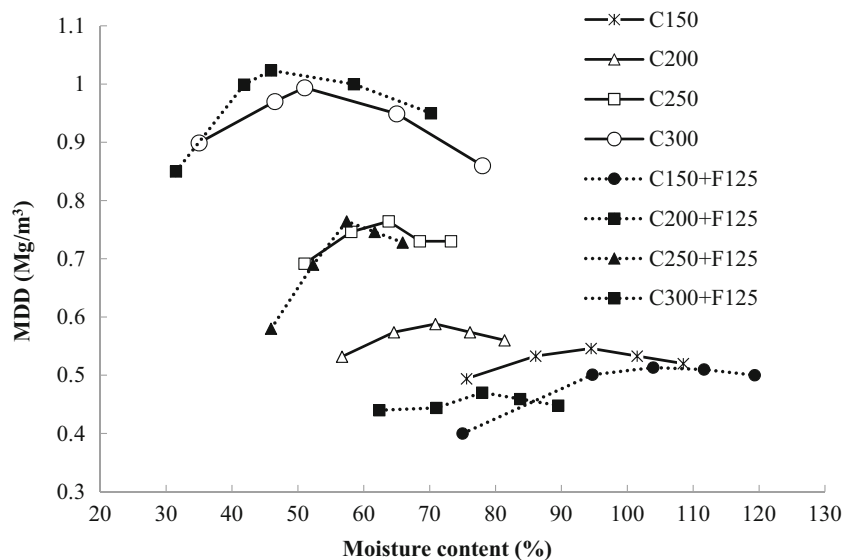
Figure 5 illustrates the variations of CBR values of cement peat with 300-kg/m<sup>3</sup> cement mixed with different dosages of

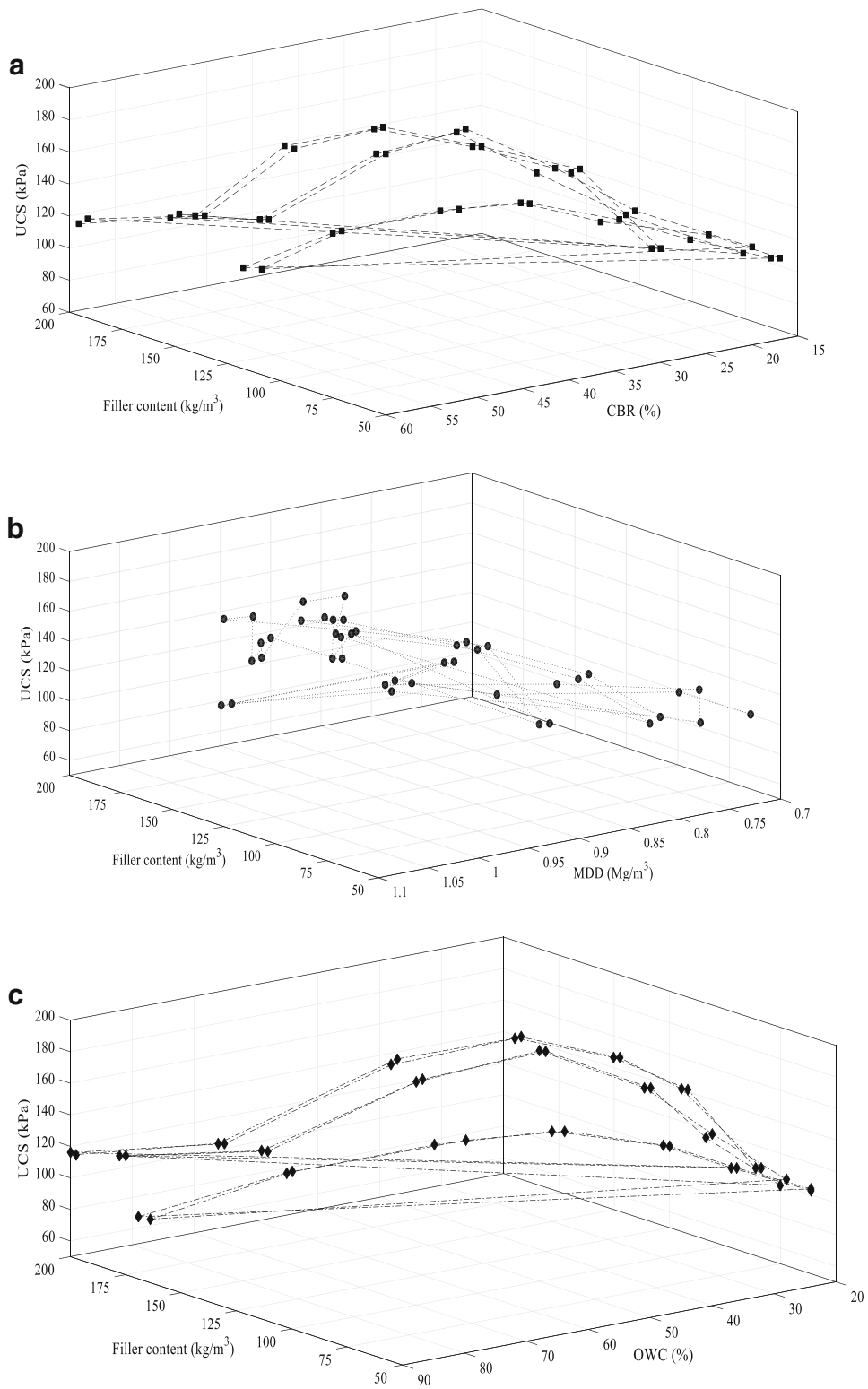
filler cured for 14, 28 and 90-day. The horizontal lines represent the CBR of peat and cement only. For standard CBR, the CBR of natural fibrous was found at 3%. This value reached to 21% using optimum cement content in 14-day curing, which is seven times higher than the original value. Over more curing time the CBR values increased to 36% and 41% in 28 and 90-day, respectively. The CBR of untreated peat showed that the soil has poor Geotechnical properties (0 to 3%). This low CBR of compared to the stabilized samples is mainly attributed to inherent low shear strength of peats which is due to high void ratio and less solid particles of these problematic soils. According to Fig.5, inclusion of the filler content

**Fig. 5** CBR values of cement peat with 300-kg/m<sup>3</sup> cement mixed with different dosages of filler cured for 14, 28 and 90 days



**Fig. 6** Maximum dry density of treated peat mixed with 125-kg/m<sup>3</sup> dosages of filler cured for 28 days





**Fig. 7** Variation of filler effect on the UCS of treated samples with (a): CBR, (b): MDD and (c): OWC

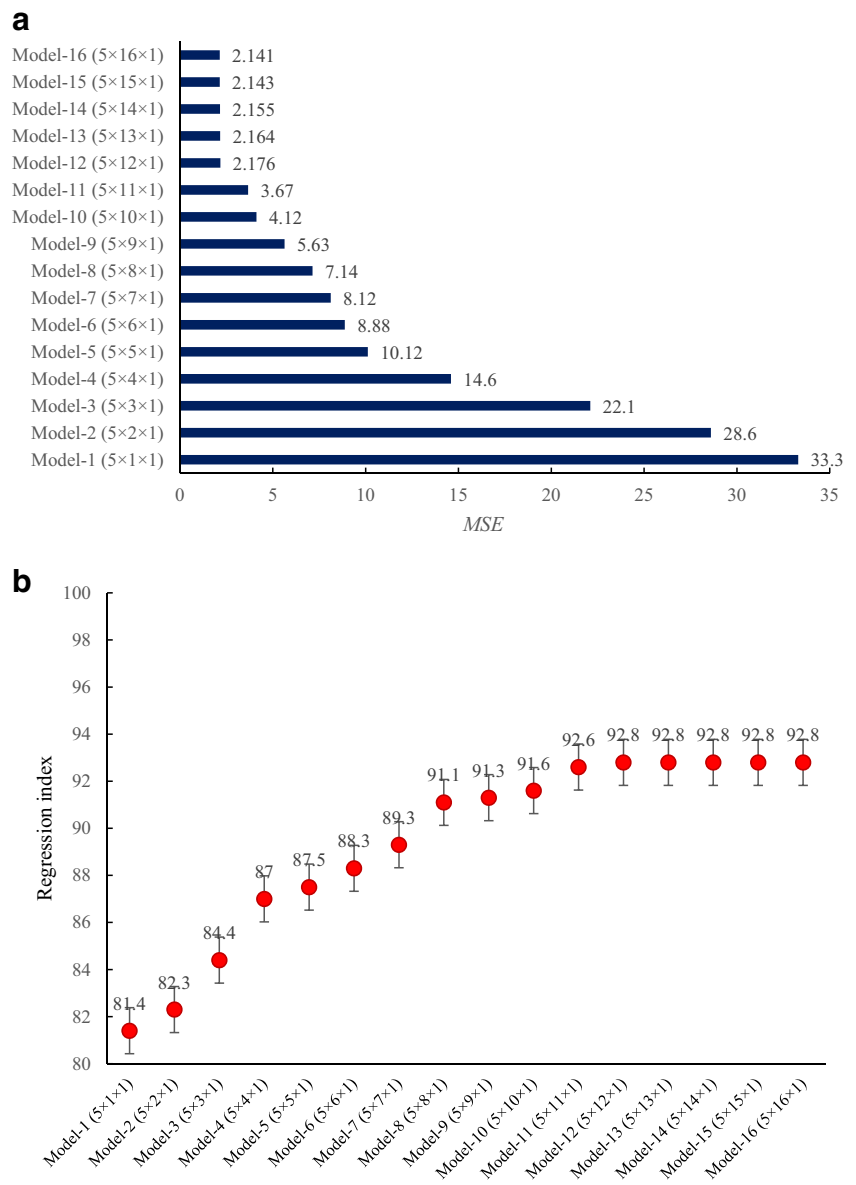


in the cement peat mixture did not show any optimum amount. By adding the filler amount from  $50 \text{ kg/m}^3$  to  $200 \text{ kg/m}^3$  the CBR values of treated peat increased sharply. For an example, using  $200 \text{ kg/m}^3$  filler in comparison of cement peat, the CBR increased from 41% to 58.6% in 90 days curing period. In comparison with untreated soil, the CBR of cement peat mixed with  $200 \text{ kg/m}^3$  filler content was increased by a factor as high as 19.4 times. The results of this analysis imply that for stabilized peat samples with more than  $200 \text{ kg/m}^3$  filler dosages, higher CBR value can be expected.

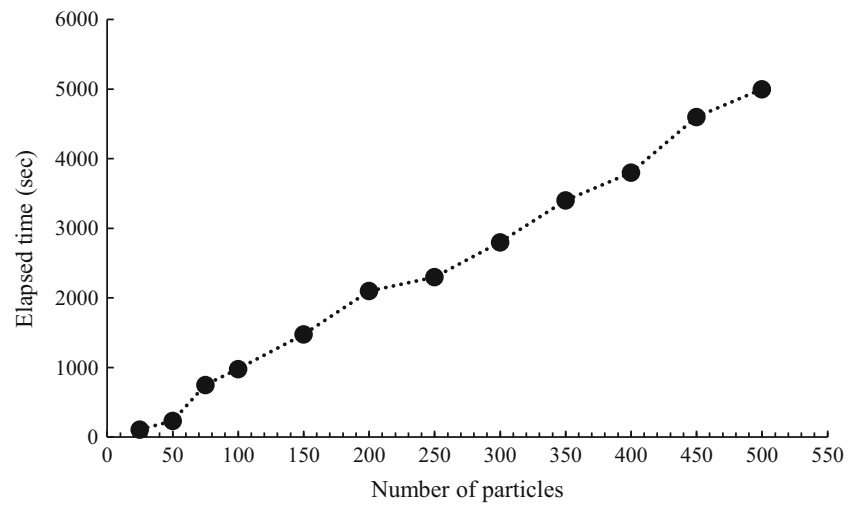
Figure 6 shows the MDD/moisture content relationship of cement peat samples and cement peat samples mixed with different filler dosages. For example, in the case of  $125\text{-kg/m}^3$  filler content, OWC and MDD for untreated

peat was found to be 135% and  $0.42 \text{ Mg/m}^3$ , respectively. It should be noticed that the trend of untreated peat in compaction tests differs from some published studies (Kolay et al. 2011). These differences can be explained by the texture of the peats which they are significantly site-dependent. As shown in Fig. 6, for peat samples treated with cement, an increase in cement content resulted in an increase of MDD and decrease in OWC. In addition, it was observed that when filler content increased, in comparison with cement peat only, the MDD increased while OWC reduced. In this case, the increase in MDD could be mainly due to increasing the solid particles of treated peat. For example, in comparison between C300 and C300 + F200, the MDD of stabilized peat increased from  $0.97 \text{ Mg/m}^3$  to  $1.03 \text{ Mg/m}^3$ , while the OWC decreased

**Fig. 8** Performance indices of ANN modes. (a) *MSE*. (b) Regression index



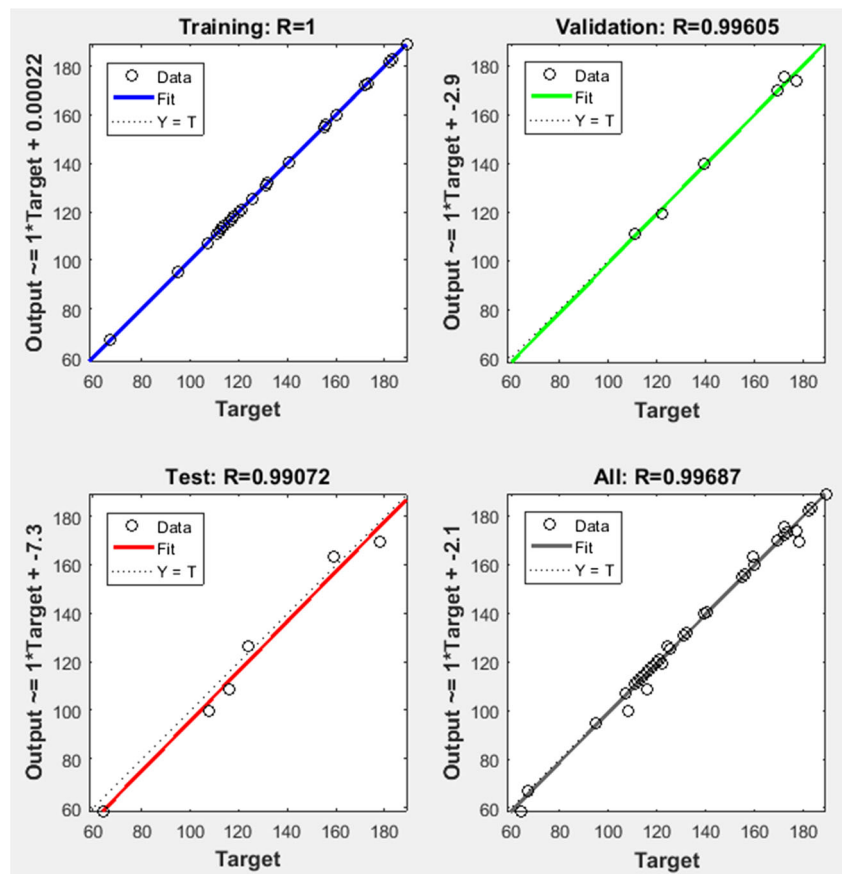
**Fig. 9** Effect of number of particles on training time of ANN-PSO model



from 51% to 45%. This decrease in OWC may be explained by the fact that, due to an increase in the solid particles in the stabilized peat samples, the number of peat particles became less. Therefore, the rate of water

absorption by peat particles decreased significantly. Finally, for the comparison purpose, Fig. 7 shows the combination effects of FC with (a): CBR, (b): MDD and (c): OWC on the UCS of treated samples.

**Fig. 10** Regression indices of the best ANN-PSO model ( $5 \times 12 \times 1$ )



**Table 5** Weights of the best ANN-PSO (input to hidden layer)

| Items | Input – 1 (CT) | Input – 2 (CBR) | Input – 3 (FC) | Input – 4 (MDD) | Input – 5 (OWC) |
|-------|----------------|-----------------|----------------|-----------------|-----------------|
| N-1   | -0.6799        | 0.3861          | 2.2683         | -0.2556         | -0.426          |
| N-2   | -2.4176        | -0.5843         | 0.3873         | -2              | -0.4817         |
| N-3   | 1.2871         | 1.305           | -1.2879        | -1.0671         | 0.7759          |
| N-4   | 1.3237         | 1.3227          | 1.9525         | -0.5788         | -1.9293         |
| N-5   | 1.6131         | 0.8813          | 0.9755         | -0.6561         | -0.0051         |
| N-6   | -0.1277        | -1.5509         | -0.2891        | 1.4241          | 0.1116          |
| N-7   | -3.0236        | 0.1245          | -1.4531        | -2.1145         | 0.8234          |
| N-8   | 1.5703         | -0.2498         | 1.1623         | -0.7946         | 0.3969          |
| N-9   | 0.0648         | -1.1734         | -1.4146        | -0.5297         | -1.3481         |
| N-10  | 1.2922         | -1.2642         | -0.3751        | 0.9055          | -0.1274         |
| N-11  | 0.7684         | -0.5837         | -1.9875        | -0.6265         | -1.128          |
| N-12  | -2.0329        | 0.4457          | 1.4819         | 0.4029          | -1.3905         |

### ANN results

As mentioned before, in the simulation process of the ANNs, just one hidden layer including different hidden neurons was used. Figure 8 a, b shows the performances of different ANN models from model-1 ( $5 \times 1 \times 1$ ) to model-16 ( $5 \times 16 \times 1$ ) trained by the BP algorithm. It should be indicated that in Fig. 9a, b the results of *MSE* and regression indices are the average of train, validation and test data. As can be seen in Fig. 8a, by increasing the number of hidden neurons from 1 to 11 the *MSE* decreased sharply, while from model-12 to model-16 approximately, the *MSE* remained constant. Moreover, increasing the number of hidden neurons more than 12 did not improved the performance of the ANN significantly. Accordingly, based on Fig. 8b, the regression indices of the models raised by the increase of the hidden neurons. Consequently, from Fig. 8a, b, the best ANN-BP model was selected as model-12 with an *MSE* = 2.143 and *R* = 92.8. After determination th of best ANN-BP model, the PSO algorithm was applied for improving the performance of the selected model. Regarding this, different swarm sizes of 25 to 500 were selected and evaluated for the training process. Meanwhile, when the swarm size (number of agents) increased, the needed time to find the

best cost function and best particle position increased, as shown in Fig. 9. Therefore, we selected 300 for the optimum number of particles. Of note, in the training process, the number of iterations was determined by trial and error tests. For example, in all models after 350 iterations, the decrease rate of cost function (*MSE*) remained constant. Besides, for the particles updating, based on suggestions of Shi and Eberhart (1999), acceleration constants were chosen as ( $C_1 = C_2 = 2$ ). Figure 10 shows the regression indices of the best ANN-PSO model. As can be seen, the average of regression indices was 1, 0.996 and 0.99 for training, validation and test data, respectively. In addition, by using the PSO learning algorithm, the average *MSE* of ANN-BP decreased from 2.143 to 0.73. It should be mentioned that the results training ANN-BP model with a PSO technique of this study was compatible with the results of previous researchers (Zhang et al. 2007; Hajihassani 2013; Sun and Xu 2016).

### Sensitivity results

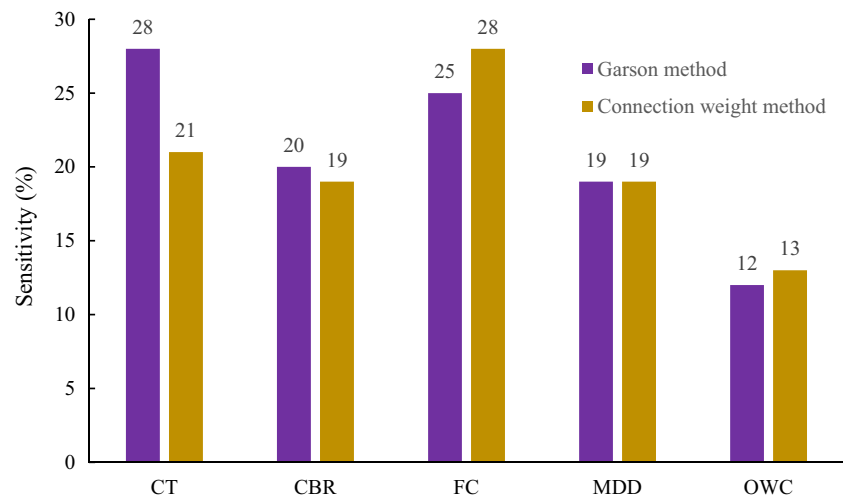
After determination of the best ANN-PSO model, the sensitivity analysis was performed using two different methods, namely Garson’s algorithm (Garson 1991) and

**Table 6** Weights of the best ANN-PSO (hidden to target layer)

| N-1   | N-2    | N-3   | N-4    | N-5   | N-6   | N-7   | N-8   | N-9   | N-10   | N-11  | N-12   |
|-------|--------|-------|--------|-------|-------|-------|-------|-------|--------|-------|--------|
| 1.014 | -0.539 | 0.496 | -0.698 | 1.012 | 0.459 | 0.602 | 0.436 | 0.467 | -0.134 | 0.368 | -0.515 |

Note: N – 1 = neuron number one

**Fig. 11** Sensitivity analysis of the best ANN-PSO model



the connection weight approach (Olden and Jackson 2002). These algorithms use the weights of input the to hidden layer and hidden to the output layer of the best ANN model. The outputs of weights and biases can be extracted by predefined commands in MATLAB software (2016). Tables 5 and 6 illustrate the details of the weights of the best ANN-PSO model of this study. Figure 11 establishes the results of aforesaid algorithms on the hidden weights of the best ANN-PSO model which is called sensitivity analysis. As can be seen, in both methods, CT and FC were introduced as the most important parameters in the estimating of UCS of treated fibrous peat. To be noticed, in reality, the texture of CBR and UCS are closer to each other in comparison with FC and CT. On the other hand, as mentioned in basic test results (Table 2), the untreated fibrous peat soil used in this study had an average void ratio of 11. Therefore, it could be expected that FC increases the UCS as high as CBR. As can be seen in Fig. 11 based on these two mentioned methods, no significant difference between parameters was seen. For example, in Garson's algorithm, just a 5% difference was observed between FC and CBR. On the other hand, it was interesting that in both methods, OWC had the minimum effect on the UCS. It can be concluded that in sensitivity analysis, both methods showed approximately similar trends.

## Conclusions

In this study, the geotechnical characteristics of cement-stabilized peat mixed with filler were investigated using UCS, CBR and compaction tests. Also, different ANN

modes trained by back-propagation and particle swarm optimization methods were utilized to estimate UCS of treated peat samples. Finally, sensitivity analysis was performed to evaluate the most important parameters on the UCS of treated samples. The results indicated that to achieve the highest undrained shear strength in the UCS tests, 300-kg/m<sup>3</sup> cement was determined as the optimum cement content at the natural water content of the peat. By using filler, the undrained shear strength of cement-treated peat increased slightly. In the cases of CBR tests, the role of filler was more comparable to the other tests. In these tests, by adding the filler content to the mixture of cement peat, the CBR values increased significantly. Additionally, in compaction tests, the MDD of cement-stabilized peat decreased with the increase in cement content while the OCW reduced. This trend repeated in the tests using filler too. Moreover, results of soft computing methods showed that ANN-PSO models had better performance than ANN-BP. The best ANN-PSO model had an  $MSE = 0.73$  and the average regression index of around one (1, 0.996 and 0.99 for training, validation and test data, respectively), showing the high performance of the model. Finally, sensitivity analysis introduced filler content and curing time as the most influential factors in the estimation of UCS of treated peat samples.

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## Compliance with ethical standards

**Conflict of interests** The authors declare that there are no conflicts of interest regarding the publication of this paper.

## Appendix

**Table 7** Database used for ANN

| Test no. | CBR (%) | CT (day) | OWC (%) | MDD (Mg/m <sup>3</sup> ) | FC (kg/m <sup>3</sup> ) | UCS (kPa) |
|----------|---------|----------|---------|--------------------------|-------------------------|-----------|
| 1        | 17      | 14       | 24      | 0.73                     | 24                      | 111       |
| 2        | 19      | 14       | 28      | 0.75                     | 28                      | 117       |
| 3        | 25      | 14       | 30      | 0.88                     | 30                      | 121       |
| 4        | 28      | 14       | 39      | 0.93                     | 39                      | 125.4     |
| 5        | 31      | 14       | 49      | 0.83                     | 49                      | 113       |
| 6        | 37      | 14       | 64      | 1                        | 64                      | 95        |
| 7        | 41      | 14       | 79      | 0.76                     | 79                      | 67        |
| 8        | 18      | 14       | 24      | 0.78                     | 24                      | 112       |
| 9        | 21      | 14       | 27      | 0.73                     | 27                      | 116       |
| 10       | 23      | 14       | 29      | 0.82                     | 29                      | 120       |
| 11       | 27      | 14       | 37      | 0.94                     | 37                      | 124       |
| 12       | 29      | 14       | 44      | 0.82                     | 44                      | 112       |
| 13       | 36      | 14       | 63      | 0.99                     | 63                      | 95        |
| 14       | 39      | 14       | 77      | 0.78                     | 77                      | 64        |
| 15       | 20      | 28       | 28      | 0.82                     | 28                      | 121       |
| 16       | 27      | 28       | 31      | 0.84                     | 31                      | 140.6     |
| 17       | 30      | 28       | 33      | 0.91                     | 33                      | 160       |
| 18       | 34      | 28       | 41      | 1.023                    | 41                      | 178       |
| 19       | 37      | 28       | 52      | 0.93                     | 52                      | 155       |
| 20       | 44      | 28       | 67      | 0.88                     | 67                      | 111       |
| 21       | 49      | 28       | 81      | 0.83                     | 81                      | 107       |
| 22       | 21      | 28       | 29      | 0.83                     | 29                      | 118       |
| 23       | 28      | 28       | 32      | 0.85                     | 32                      | 139       |
| 24       | 32      | 28       | 32      | 0.92                     | 32                      | 159       |
| 25       | 35      | 28       | 40      | 1                        | 40                      | 177       |
| 26       | 38      | 28       | 51      | 0.94                     | 51                      | 156       |
| 27       | 45      | 28       | 68      | 0.89                     | 68                      | 112       |
| 28       | 48      | 28       | 82      | 0.82                     | 82                      | 108       |
| 29       | 30      | 90       | 32      | 0.93                     | 32                      | 131       |
| 30       | 33      | 90       | 36      | 0.94                     | 36                      | 173       |
| 31       | 38      | 90       | 37      | 1.02                     | 37                      | 182       |
| 32       | 43      | 90       | 44      | 1.1                      | 44                      | 189       |
| 33       | 47      | 90       | 56      | 1.02                     | 56                      | 169       |
| 34       | 51      | 90       | 74      | 0.97                     | 74                      | 121       |
| 35       | 58      | 90       | 90      | 0.9                      | 90                      | 116       |
| 36       | 31      | 90       | 33      | 0.94                     | 33                      | 132       |
| 37       | 34      | 90       | 35      | 0.95                     | 35                      | 172       |
| 38       | 39      | 90       | 38      | 1.04                     | 38                      | 183       |
| 39       | 44      | 90       | 45      | 0.98                     | 45                      | 189       |
| 40       | 48      | 90       | 55      | 0.97                     | 55                      | 172       |
| 41       | 52      | 90       | 75      | 0.96                     | 75                      | 122       |
| 42       | 59      | 90       | 89      | 0.91                     | 89                      | 114       |

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